

Technical Notes

Evaluation of Shear Wave Velocity Correlations and Development of New Correlation Using Cross-hole Data

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Abstract: Seismic microzonation studies are being proposed in Pakistan. In addition, a downhole array of accelerometers was planned to be installed in the University of Engineering and Technology, Mardan Campus. Therefore, extensive geotechnical and geophysical tests were conducted. Shear wave velocity (V_s) is a fundamental parameter required for these microzonation studies. It is feasible in terms of cost and space to determine V_s from Standard Penetration Test (SPT) or Cone Penetration Test (CPT) results through empirical correlations. The purpose of this paper is to explore the applicability and predictability of these correlations to the data collected from the area where downhole array is planned. Data from these surveys was used to evaluate relevant correlations selected from literature. Predicted shear wave velocity values from these correlations were compared with measured shear wave velocity values from seismic crosshole tests. Most SPT- V_s correlations evaluated showed low predictability. The SPT- V_s correlation that showed highest degree of fitness to the dataset was the one developed for Lucknow, India, a city with similar geological setting, workmanship and SPT method employed. Site specific SPT- V_s correlation was also proposed. Most of the CPT- V_s correlations evaluated showed considerable predictive capability compared to the SPT- V_s correlations.

Keywords: microzonation, shear wave velocity, cross-hole, geophysical, standard penetration

1 Introduction

Pakistan is an earthquake prone country. It is located at the Himalayan Plate Boundary. Almost two-thirds of the area of the entire country is located on fault lines. Over the past 100 years, this region has been hit by some of the most disastrous earthquakes ever recorded, including the 1935 Quetta earthquake (Moment Magnitude, $M_w = 7.5$), 1945 Makran Coast earthquake ($M_w = 8$), 1974 Hunza earthquake ($M_w = 6.2$) and 2005 Kashmir earthquake ($M_w = 7.6$). A number of microzonation studies are being proposed for different parts of the region. The V_s of soil is an important input into these studies. V_s is a fundamental soil parameter used in soil classification, stratigraphy, determination of

liquefaction potential, site response analysis, etc. V_s is preferably measured through in situ seismic non-destructive tests such as crosshole seismic testing, downhole/uphole methods and multi-channel analysis of surface waves (MASW). However, the application of these methods is infeasible due to cost and space constraints. Therefore, empirical correlations have been developed to determine V_s from more simple and common tests such as the SPT and CPT.

SPT is a simple test in geotechnical engineering in which a tube attached to drill rods is driven into the soil down to a distance of 45 cm in three successive increments of 15 cm by a hammer weighing 63.5 kg falling over an anvil through a distance of 76 cm. The number of

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blows recorded is reported as the SPT blow count (SPT-N). A number of design parameters depend on the SPT-N values. Since as early as the 1960's, extensive research has been conducted to develop empirical relationships between V_s and SPT-N and a number of correlations are available in literature (Kanai 1966, Imai 1977, Ohta and Goto 1978, Imai and Tonouchi 1982 Seed et al 1983, Sykora and Stokoe 1983, Kalteziotis et al 1992, Sisman 1995, Pitilakis et al 1999, Kiku et al 2001, Jafari et al 2002, Hasançebi and Ulusay 2007, Dikmen 2009, Uma Maheswari et al 2010, Tsiambaos and Sabatakakis 2011, Anbazhagan et al 2012, Shahzada et al 2012, Fauzi et al 2014). These correlations have been developed for different types of soils. Most of these correlations were developed for uncorrected SPT values.

The Cone Penetration Test (CPT) is another common in situ method employed for accurate determination of soil stratigraphy, soil type, lithologic anomalies and some other soil geotechnical parameters. In the conventional CPT test, a standard instrumented cone is vertically forced into the soil at controlled rate. The tip resistance (q_c), sleeve friction (f_s) and pore water pressure (u) are recorded. This test gives continuous, reliable and repeatable results. Extensive research, since as early as the 1980's, has been conducted to develop correlations between CPT results and V_s (Baldi et al 1989, Robertson 1990, Hegazy and Mayne 1995, Mayne and Rix 1995, Mayne 2006, Mayne 2007, Andrus et al 2007, Robertson 2009). These correlations have been developed for different types of soils.

Mardan is a central city of the earthquake-prone province of Khyber Pakhtunkhwa in Pakistan. Mardan is classified in seismic zone 2B according to Building Code of Pakistan (Seismic Provisions-2007). Extensive geotechnical and geophysical investigations were carried out as a prerequisite to a comprehensive program of deploying seismic accelerometer arrays in Mardan. Included in these tests were SPT, CPT, seismic crosshole test (CH), MASW, cyclic triaxial tests, resonant column tests, etc. In this study, the data from these investigations was used to evaluate relevant SPT- V_s and CPT- V_s correlations from literature. V_s values measured

through CH were used to determine the predictive capability of these correlations. Except for the work of Shahzada et al (2012), little or no research has been done on the subject to develop correlations meeting the geological setting of Pakistan. Shahzada et al (2012) correlated SPT-N values with V_s obtained from MASW. Whereas in this study, SPT-N values were correlated with V_s obtained seismic crosshole test (CH), which is a more reliable test than MASW (Anderson et al 2007). New empirical correlations for SPT- V_s and CPT- V_s have been proposed herein and compared to the selected existing correlations. The degree of fitting of all existing and proposed regression equations was evaluated through statistical analysis.

2 Site Geology and Seismotectonics

Several segments of the Himalayan plate boundary in Pakistan have active faults including the Chaman fault, Kingri Fault, Kalabagh fault, Ornach Nal fault and the Main Mantle Thrust (MMT). The MMT has shown recent activity as breaks in the overlying alluvium and terraces have been observed. The site chosen for this study is located at Mardan. Mardan is one of the major cities of the Khyber Pakhtunkhwa province of Pakistan. Seismotectonic map highlighting the faults in the surrounding areas of Mardan is given in Fig. 1.

Mardan is located in the Peshawar Basin. The Peshawar Basin covers a part of the Himalayan fold-and-thrust belt, it is believed to have been carried passively on the back of low angle detachment faults and thrust sheets, some of which find surface expression in hill ranges to the south of the basin. It is thus classified as a piggyback-type basin. The Peshawar Basin covers a vast area (over 5,500 km²), having besides Mardan, Charsadda, Noshera and Peshawar as its major cities. It is situated at the southern margin of Himalayas and bounded by the Khyber ranges in the west/northwest, Attock cherat ranges in the South and Swat in the North/Northeast. Quaternary fanglomerates form the basin margins, whereas fluvial micaceous sands, gravels and lacustrine deposits cover its central part. The fluvial deposits have a northern

provenance and were probably deposited by the ancestral Kabul and Indus Rivers. However, in the southern part of the basin, fanglomerate and lacustrine deposits have been apparently derived from the Attock-Cherat and adjacent ranges.

Mardan is divided into the north-eastern hilly area and the south-western plain. The northern region is bounded by hills with highest peaks of Pajja and Garo measuring 2056 m and 1816 m

high, respectively. The southwestern plain is accepted to have once formed the bed of a lake which was gradually filled up with deposits of rivers falling in from the northwestern hills. Most of the area of the city is waterlogged and underlain by Holocene and Quaternary alluvial deposits. With a population of over 2 million, the city is now developing into an urban center in the province.

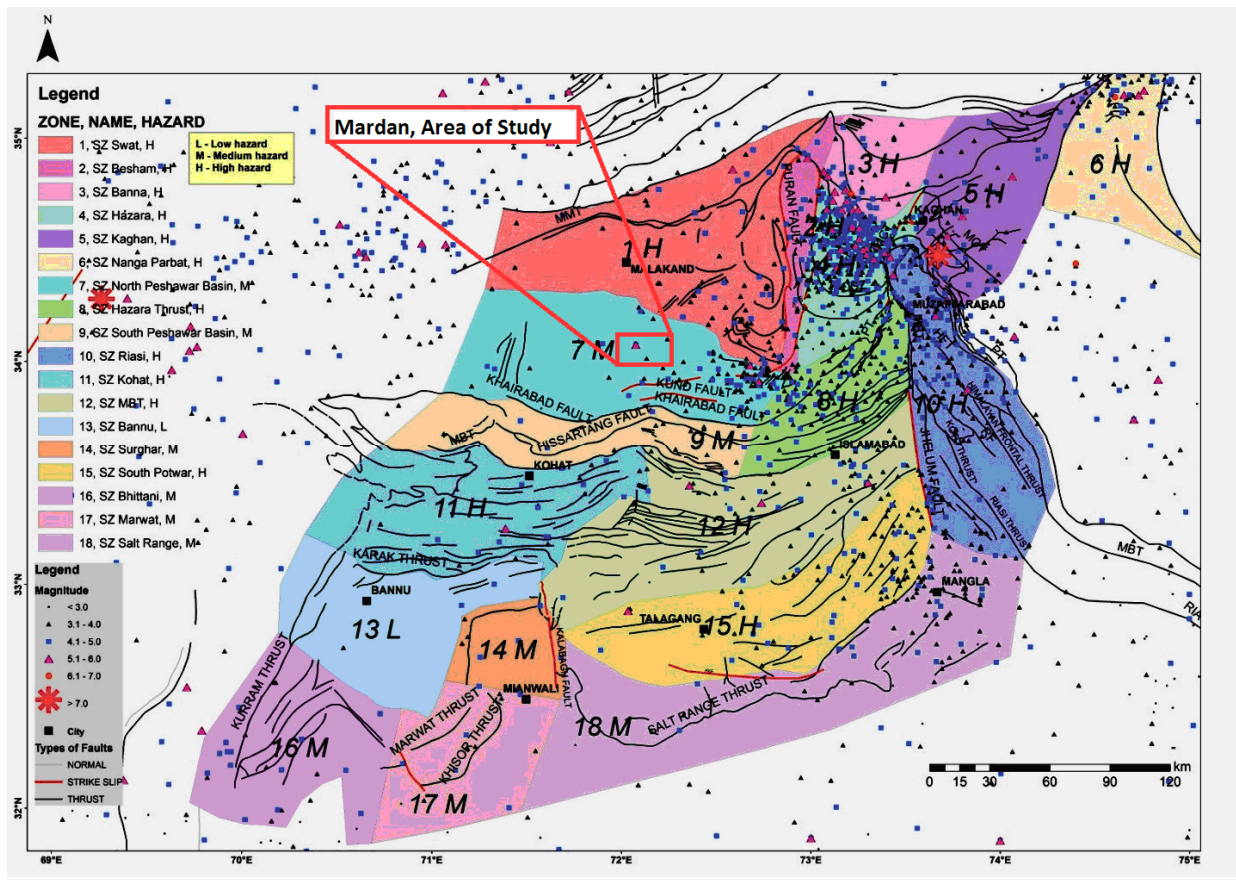


Fig. 1 Seismotectonic zonation map of the NW Himalayan Fold-and-Thrust Belt (MonaLisa et al 2009)

3 In situ tests and subsurface conditions

Three boreholes were drilled in line, each 1 m apart. The central borehole was 100 m deep while the other two were 50 m deep. SPT was conducted in all three boreholes. Donut hammer with a rope and pulley system was used for SPT measurements. A total of 86 SPT measurements were recorded up to a depth of 100 m. In addition, a total of 32 disturbed and 21 undisturbed samples were collected from the boreholes for laboratory testing. A variety of laboratory tests were performed over these samples for the determination of moisture content, Atterberg’s

limits, specific gravity, consolidation, grain size analysis, etc. To determine the dynamic soil properties, undisturbed samples were used for resonant column and cyclic triaxial tests. Average SPT-N variation with depth up to 50 m in the three boreholes is shown in Fig. 2. CPT measurements were recorded up to a depth of 23 m (Fig. 3). Seismic crosshole test was performed for determining Vs variation within the soil profile along the depth. Measurements were made at every meter up to a depth of 50 m. Variation of measured shear wave velocity along the depth is shown in Fig. 4.

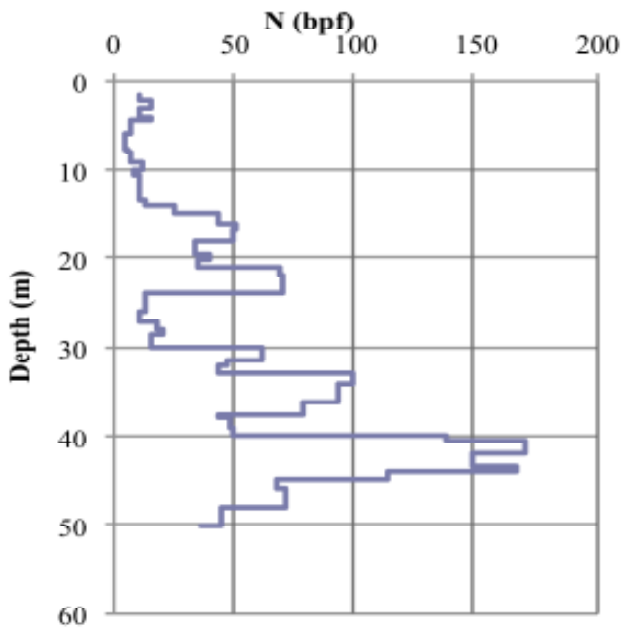


Fig. 2 Variation of average SPT-N value with depth

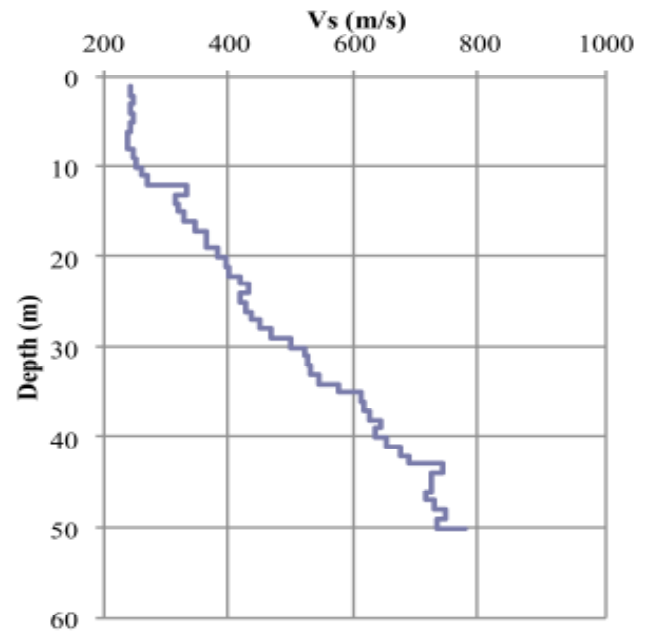


Fig. 4 Variation of Vs measured from CH with depth

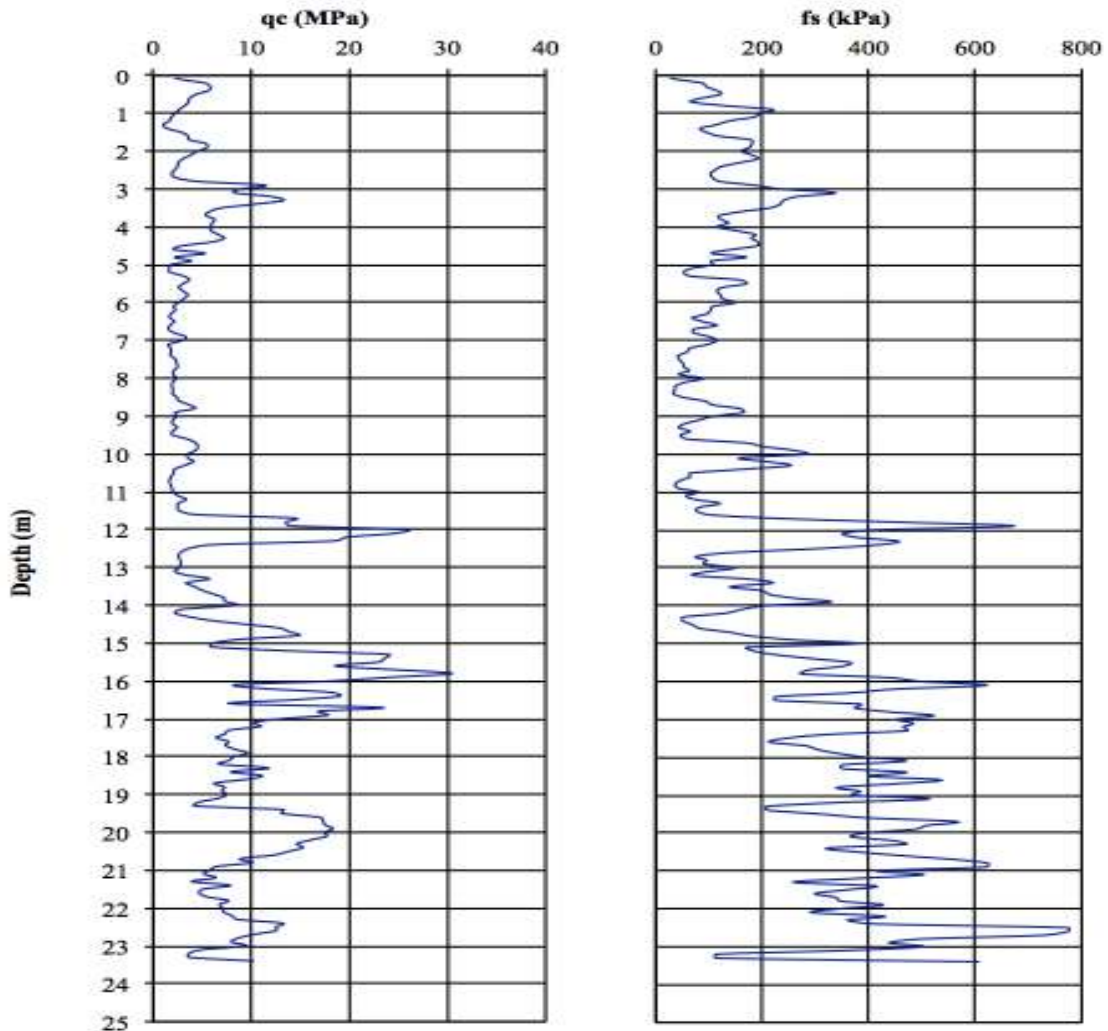


Fig. 3 Variation of qc and fs measured from CPT with depth

The soil profile was highly variable in terms of soil type. Up to a depth of 30 m, intermittent layers of deposits of clay, silty clay and silt were found with low to medium plasticity. Ground water table was encountered at a depth of 4.7 m. From about 30-50 m, soil predominantly composed of layers of stiff silty clay with thin layers of soft silt. The stiff silty clay was grayish brown in color, saturated, contained traces of fine sand and had medium to high plasticity. From 40-45 m, highly stiff soil was encountered containing pieces of mudstone. Minimum plasticity index of 4.2% was observed in the superficial alluvial layers and maximum plasticity index of 15.5% was observed at a depth of 34 m in the stiff silty clay layer. For soil classification, shear wave velocity averaged over 30 m depth (V_{s30}) was found to be equal to 323 m/s. Under the Caltrans/NEHRP soil classification system, the site class for the studied soil profile was D (Stiff Soil).

4 Evaluation of SPT-Vs Correlations

Of many correlations in literature between shear wave velocity and SPT-N, 12 correlations were selected for evaluation. These correlations were selected on the basis of similarities between soil type and age of the study site and those of the original datasets upon which the correlations were based. Details of these correlations are given in Table 1. The SPT and V_s obtained from CH data collected at Mardan in this study was used to evaluate the performance of these existing correlations. All of these correlations were developed using uncorrected SPT-N values.

The scatter of points shown in Fig. 5 indicates the data pairs of uncorrected SPT-N values and measured values of V_s along the depth. Each of the selected correlations was used to predict V_s for every SPT-N value. The measured and predicted values of V_s were used to determine the degree of fitness of each correlation in terms of R-squared value (R^2), root mean square deviation (RMSD) and coefficient of variance of RMSD (CVRMSD). A summary of the selected correlations and their degrees of fitness to the dataset of the study site is given in Table 2. Most of the selected correlations underpredict shear wave velocity for SPT-N values greater than 50.

Correlation by Anbazhagan et al (2012) shows the greatest degree of fitness to the dataset with R^2 value of 0.45.

5 Evaluation of CPT-Vs Correlations

Four empirical regression equations correlating CPT results with V_s were selected from literature. The details of these correlations are given in Table 1. The input parameters for predicting V_s were q_c , f_s and depth (z). The values of V_s predicted from selected correlations were compared with V_s measured values from the study site. Figure 6 shows the plots of measured V_s values and those predicted by the selected correlations. The degree of fitness was determined in terms of R^2 , RMSD and CVRMSD. A summary of the selected correlations and their degrees of fitness to the dataset for the study site is given in Table 3. It was observed that equations developed by Mayne (2006) and Piratheepan (2002) showed greatest predictive capability with R^2 values of 0.933 and 0.824 respectively. Piratheepan's (2002) proposed correlations were based on CPT data collected from the United States, Canada and Japan. The correlation was originally developed for Holocene clayey soils and a total of 20 data pairs were used. Mayne (2006) proposed a correlation for a large dataset collected from worldwide sites. The regression equation was developed for all soils using 161 data pairs. Since the existing correlations showed substantial fitness to the dataset used in this study, no new correlations were proposed.

6 Proposed correlation between SPT N and Shear wave velocity

To take into account the effect of indigenous SPT hammers used, workmanship and geology, a dedicated correlation was developed. Sixty-seven data pairs between uncorrected SPT-N values and measured values of V_s were used for developing statistical correlations between the two parameters. Uncorrected SPT-N values were used for the development of this correlation because they have major effect in estimation of V_s (Dikmen 2009). The following two models were selected for developing correlations between SPT-N and V_s :

Table 1 Summary of existing relevant SPT-Vs and CPT-Vs selected for evaluation

| S.N. | Authors | Original Equations | Remarks |
|----------------------------|----------------------------------|--|---|
| SPT-Vs Correlations | | | |
| 1 | Uma Maheswari et al (2010) | $V_s = 89.31 N^{0.358}$ | Developed for Cohesive Soils - Vs determined from MASW |
| 2 | Dikmen (2009) | $V_s = 44 N^{0.48}$ | Developed for Cohesive Soils - Vs determined from field geoseismic tests |
| 3 | Hasancebi and Ulusay (2007) | $V_s = 97.89 N^{0.269}$ | Developed for Cohesive Soils - Vs found from field geoseismic tests |
| 4 | Jafari et al (2002) | $V_s = 27 N^{0.73}$ | Developed for Cohesive Soils - Vs from seismic refraction, downhole and SASW |
| 5 | Raptakis et al (1995) | $V_s = 184.2 N^{0.17}$ | Developed for Cohesive Soils using geophysical tests for Vs |
| 6 | Kalteziotis et al (1992) | $V_s = 76.6 N^{0.45}$ | Developed for Cohesive using geophysical tests for Vs Soils |
| 7 | Lee (1990) | $V_s = 114.43 N^{0.31}$ | Developed for Cohesive Soils – Vs from seismic downhole tests |
| 8 | Japan Road Association (1980) | $V_s = 100 N^{0.33}$ | Developed for Cohesive Soils using geophysical tests for Vs |
| 9 | Anbazhagan et al (2012) | $V_s = 106.63 N^{0.39}$ | Developed for Cohesive Soils - Modified previous correlations to suit indigenous setting |
| 10 | Seed et al (1983) | $V_s = 56.4 N^{0.5}$ | Developed for Cohesionless Soils using geophysical tests for Vs |
| 11 | Imai (1977) | $V_s = 102 N^{0.242}$ | Developed for Cohesive Soils using geophysical tests for Vs |
| 12 | Tsiambaos and Sabatakakis (2011) | $V_s = 88.8 N^{0.370}$ | Developed for Cohesive Soils – Vs from seismic crosshole tests |
| CPT-Vs Correlations | | | |
| 1 | Hegazy and Mayne (1995) | $V_s = (10.1 \log(qc) - 11.4)^{1.67} (100fs/qc)^{0.3}$ | Developed for All Soils- Based on data from 61 sites worldwide |
| 2 | Mayne (2006) | $V_s = 118.8 \log(fs) + 18.5$ | Developed for All Soils |
| 3 | Piratheepan (2002) | $V_s = 32.2 qc^{0.089} fs^{0.121} D^{0.215}$ | Developed for All Soils- Based on data collected from the United States, Canada and Japan |
| 4 | Piratheepan (2002) | $V_s = 11.9 qc^{0.269} fc^{0.108} D^{0.127}$ | Developed for Clay- Based on data collected from the United States, Canada and Japan |

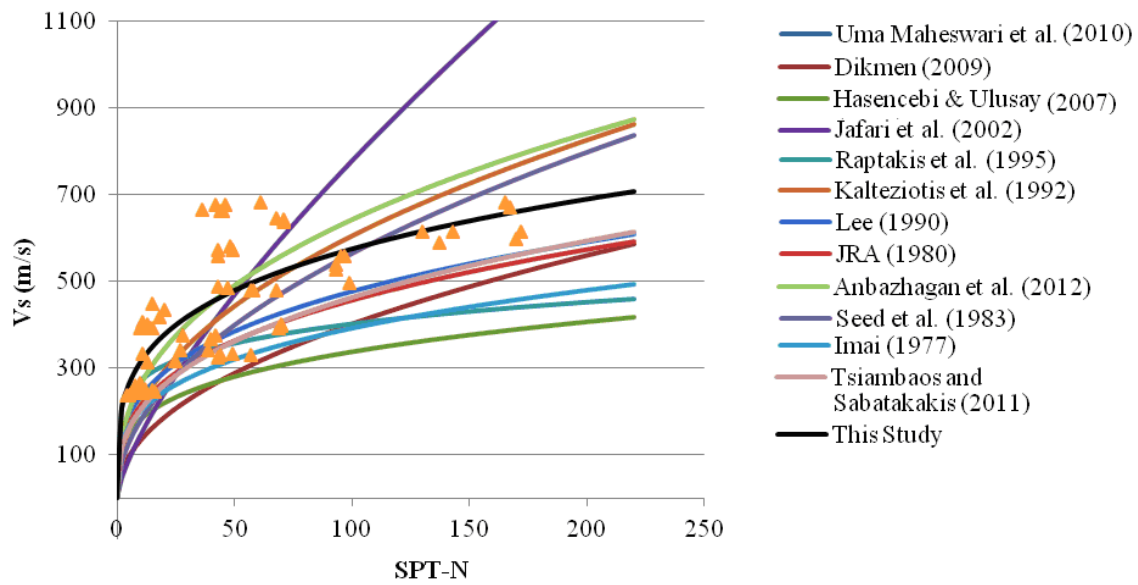


Fig. 5 Comparison of Vs values predicted from SPT-Vs correlations and Vs measured by CH

Table 2 Degree of fitness of evaluated SPT-Vs correlations to the dataset from study site

| S.N. | References | Correlation of Vs (m/s) | RMSD | CVRMSD | R ² |
|------|----------------------------------|-------------------------|------|--------|----------------|
| 1 | Uma Maheswari et al (2010) | $V_s = 89.31 N^{0.358}$ | 138 | 0.31 | 0.13 |
| 2 | Dikmen (2009) | $V_s = 44 N^{0.48}$ | 206 | 0.47 | -0.93 |
| 3 | Hasancebi and Ulusay (2007) | $V_s = 97.89 N^{0.269}$ | 212 | 0.48 | -1.05 |
| 4 | Jafari et al (2002) | $V_s = 27 N^{0.73}$ | 209 | 0.47 | -0.98 |
| 5 | Raptakis et al (1995) | $V_s = 184.2 N^{0.17}$ | 153 | 0.35 | -0.07 |
| 6 | Kalteziotis et al (1992) | $V_s = 76.6 N^{0.45}$ | 120 | 0.27 | 0.34 |
| 7 | Lee (1990) | $V_s = 114.43 N^{0.31}$ | 131 | 0.30 | 0.21 |
| 8 | Japan Road Association (1980) | $V_s = 100 N^{0.33}$ | 146 | 0.33 | 0.03 |
| 9 | Anbazhagan et al (2012) | $V_s = 106.63 N^{0.39}$ | 110 | 0.25 | 0.45 |
| 10 | Seed et al (1983) | $V_s = 56.4 N^{0.5}$ | 139 | 0.32 | 0.12 |
| 11 | Imai (1977) | $V_s = 102 N^{0.242}$ | 179 | 0.41 | -0.46 |
| 12 | Tsiambaos and Sabatakakis (2011) | $V_s = 88.8 N^{0.370}$ | 138 | 0.31 | 0.13 |

Table 3 Degree of fitness of evaluated CPT-Vs correlations to the dataset from study site

| S.N. | Reference | Correlation for Vs (m/s) | RMSD | CVRMSD | R ² |
|------|------------------------|--|------|--------|----------------|
| 1 | Hegazy and Mayne(1995) | $V_s = (10.1 \log(qc) - 11.4)^{1.67} (100fs/qc)^{0.3}$ | 69 | 0.159 | 0.77 |
| 2 | Mayne (2006) | $V_s = 118.8 \log(fs) + 18.5$ | 37 | 0.086 | 0.93 |
| 3 | Piratheepan (2002) | $V_s = 32.2 qc^{0.089} fs^{0.121} D^{0.215}$ | 80 | 0.185 | 0.69 |
| 4 | Piratheepan (2002) | $V_s = 11.9qc^{0.269} fc^{0.108} D^{0.127}$ | 61 | 0.141 | 0.82 |

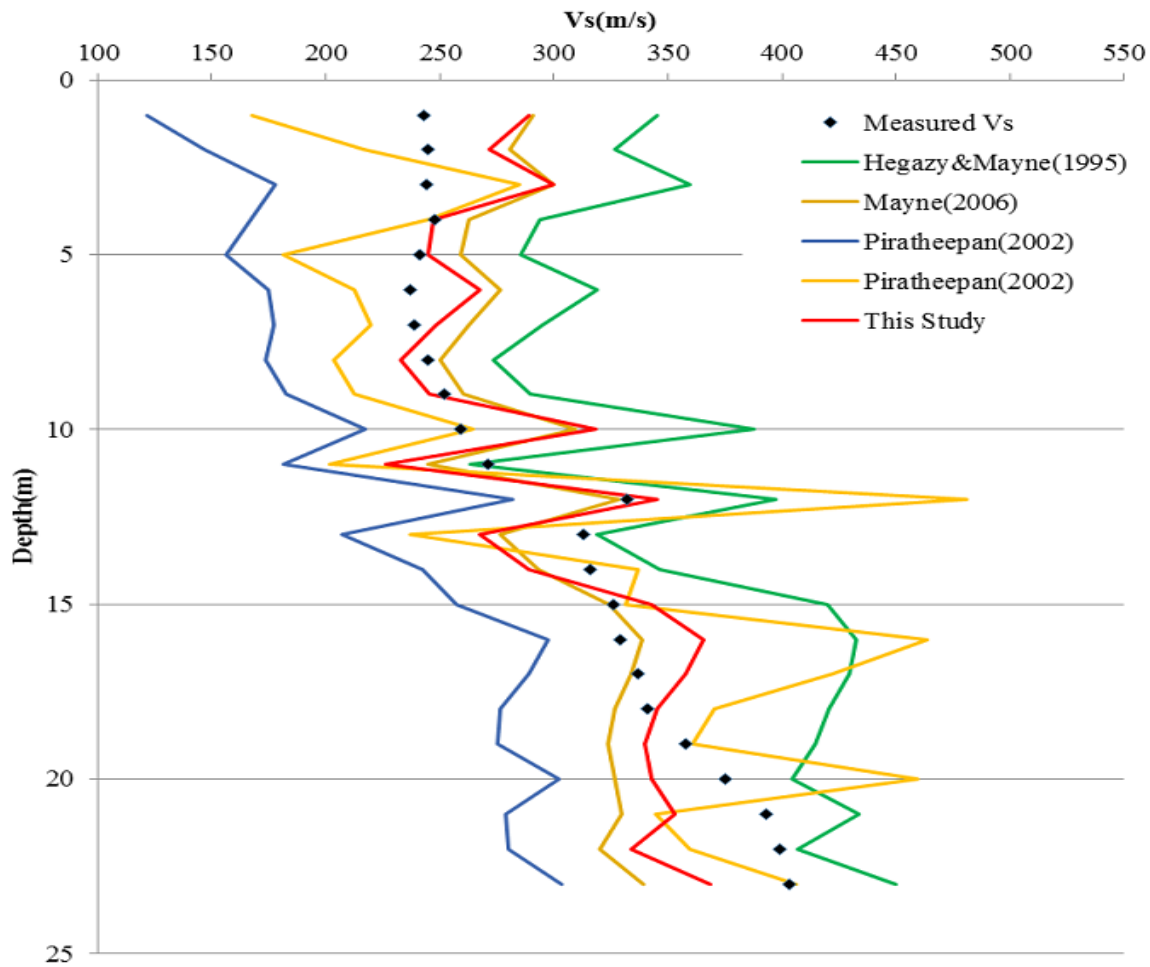


Fig. 6 Comparison of Vs predicted from CPT-Vs correlations and Vs measured by CH

Table 4 Degree of fitness of proposed correlations to the dataset from study site

| S.N. | Correlation for Vs (m/s) | RMSD | CVRMSD | R ² |
|------|----------------------------------|------|--------|----------------|
| 1 | $V_s = 82.384N^{0.047}z^{0.475}$ | 41 | 0.09 | 0.92 |
| 2 | $V_s = 171.02N^{0.263}$ | 96 | 0.22 | 0.58 |

$$V_s = aN^b z^c \tag{1a}$$

$$V_s = dN^e \tag{2a}$$

where a, b, c and d are coefficients, z is the depth and N is uncorrected SPT-N. Model (1a) was selected to account for the overburden effects and the SPT-N variation. In Fig. 4, it can be seen clearly that the Vs varies almost linearly with depth. Model (2a) was selected because the uncorrected SPT-N values inherently account for overburden effects. Nonlinear regression was

performed for the two models using least squares analysis. The equations developed were as follows:

$$V_s = 82.384N^{0.047}z^{0.475} \tag{1b}$$

$$V_s = 171.02N^{0.263} \tag{2b}$$

A summary of the degree of fitness of these equations is given in Table 4. Eq. (1b) is more sensitive to depth (z) than the SPT-N value (N). This high depth-sensitivity is attributed to the almost linear variation of Vs after 10 m.

7 Conclusion

Most of the selected correlations underpredicted the V_s values when SPT-N values exceeded 50. Least predictability was observed for the correlation developed by [Hasancebi and Ulusay \(2007\)](#) with R^2 and CVRMSD equal to -1.05 and 0.48 respectively. This correlation was based on geotechnical and geoseismic tests conducted at a first degree earthquake zone in Turkey. In addition, 8 out of the 12 correlations had R^2 values less than 0.20. This lack of agreement between the predicted and measured values demonstrates the effects of differences in geotechnical characteristics of the study area, geological age, water table effects, over-consolidation effects, etc. The variability could also be due to differences in methods of SPT employed, equipment and workmanship. Correlation developed by [Anbazhagan et al \(2012\)](#) had the greatest degree of fitness to the data pairs of SPT-N and V_s used in this study. This study was performed in Lucknow, India. It is worth noting that India and Pakistan, being neighboring countries, share much of their geological and geotechnical characteristics, SPT hammer characteristics and workmanship. Moreover, the authors classify the sites of their study as C and D based on NEHRP classification system, which is comparable to our site, classified as D under NEHRP soil classification system.

The empirical correlations proposed in this study provide the best fit for the dataset. Eq. (1b) involves a depth factor in addition to the SPT-N parameter. Because the values of V_s from this equation are more sensitive to depth than SPT-N values, this equation will overpredict V_s of any soft soil stratum if encountered at a larger depth. Soft soil layers and their accurate characterization have key role in site response analysis. Therefore, it is recommended that if the SPT-N values increase linearly with depth, Eq. (1b) should be used. However, if SPT-N values do not increase with depth and layers of soft soil are encountered at larger depths, the use of Eq. (2b) is recommended.

All of the CPT- V_s correlations evaluated showed considerable fitness to the dataset of the site of study. Correlation developed by [Mayne \(2006\)](#) showed the greatest predictive capability

with an R^2 value of 0.93. Since this equation show sufficient fitness to the dataset, therefore its use is recommended.

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